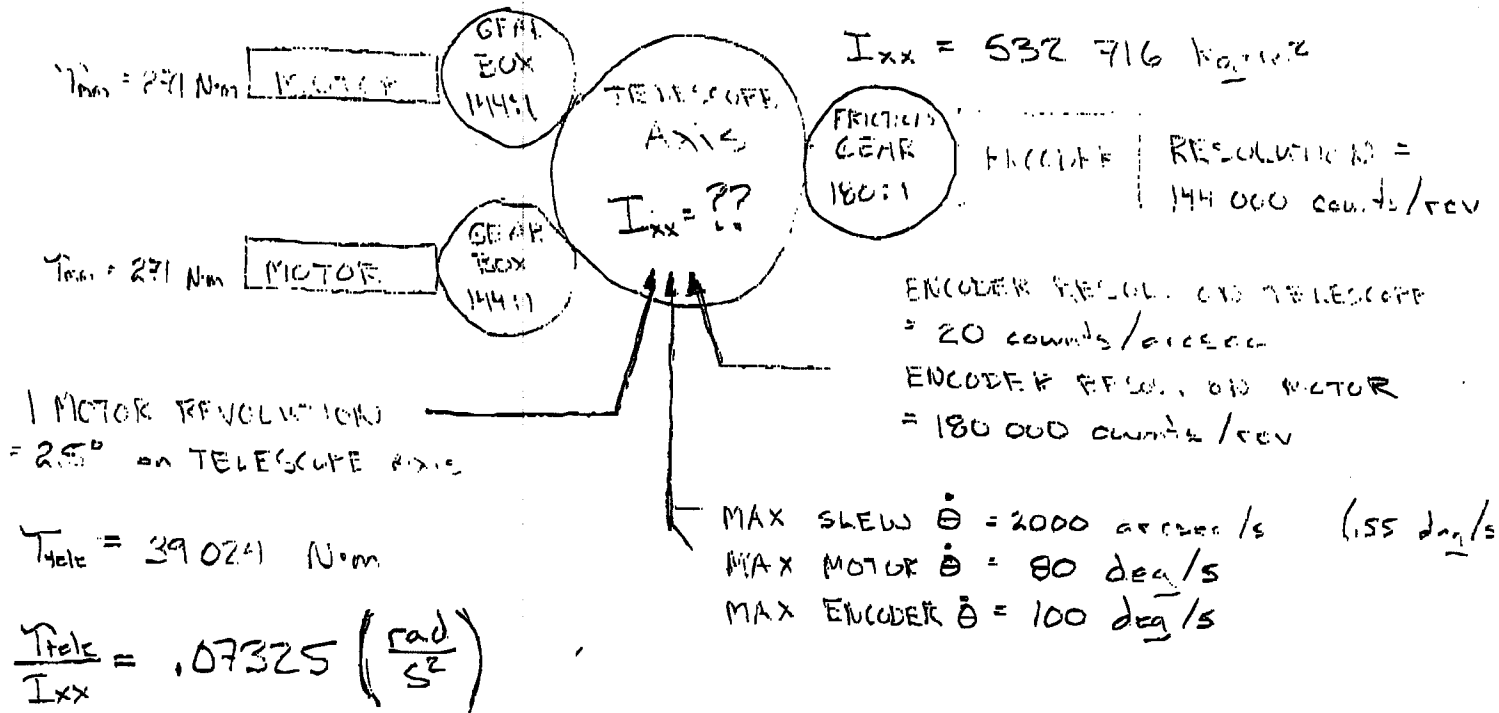
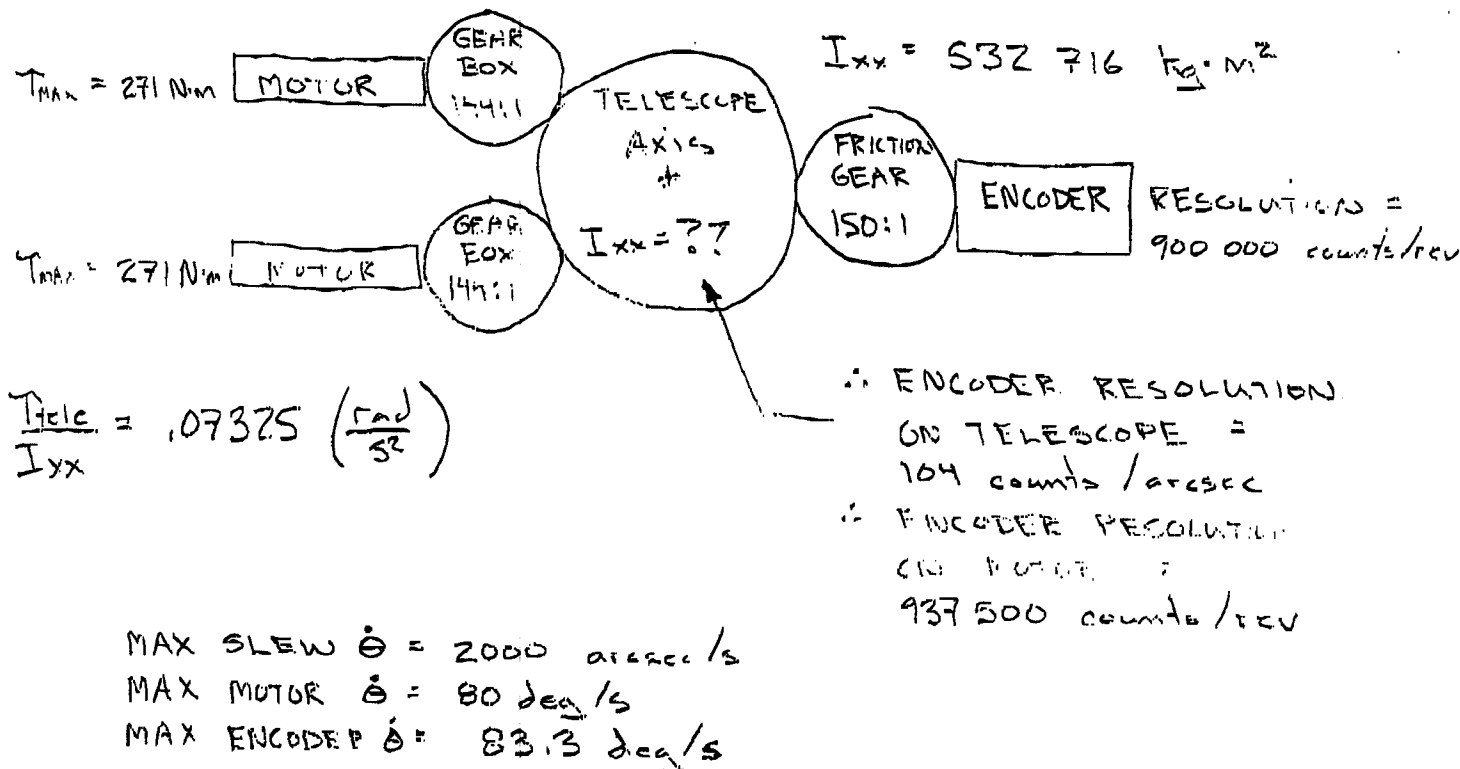


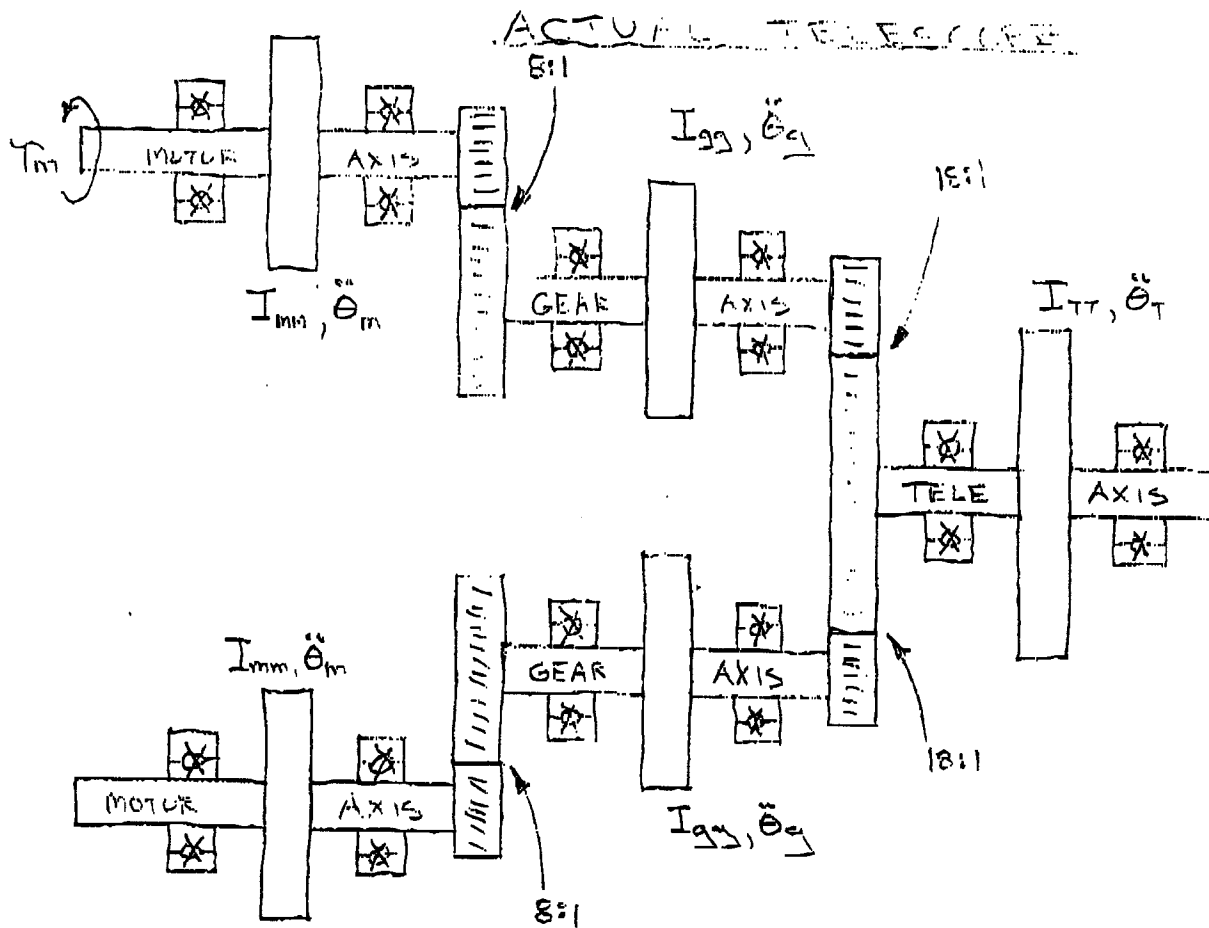
CURRENT CONFIGURATION



PROPOSED CONFIGURATION #1



①



$$T_m = \left\{ 2 \times I_{mm} + 2 \times \left(\frac{1}{8}\right)^2 I_{gg} + \left(\frac{1}{8}\right)^2 \left(\frac{1}{18}\right)^2 I_{tt} \right\} \ddot{\theta}_m$$

- \*  $T_m = 271 \text{ Nm}$  [max torque of telescope drive motor]
- \*  $I_{mm} = 0.727 \text{ kg}\cdot\text{m}^2$  [from shop drawings: shaft, coupling and motor rotor]
- \*  $I_{gg} = 8.002 \text{ kg}\cdot\text{m}^2$  [from shop drawings: 2 gears and shaft]
- \*  $I_{tt} = 532.716 \text{ kg}\cdot\text{m}^2$  [from IPL estimates] Yoke + Tube

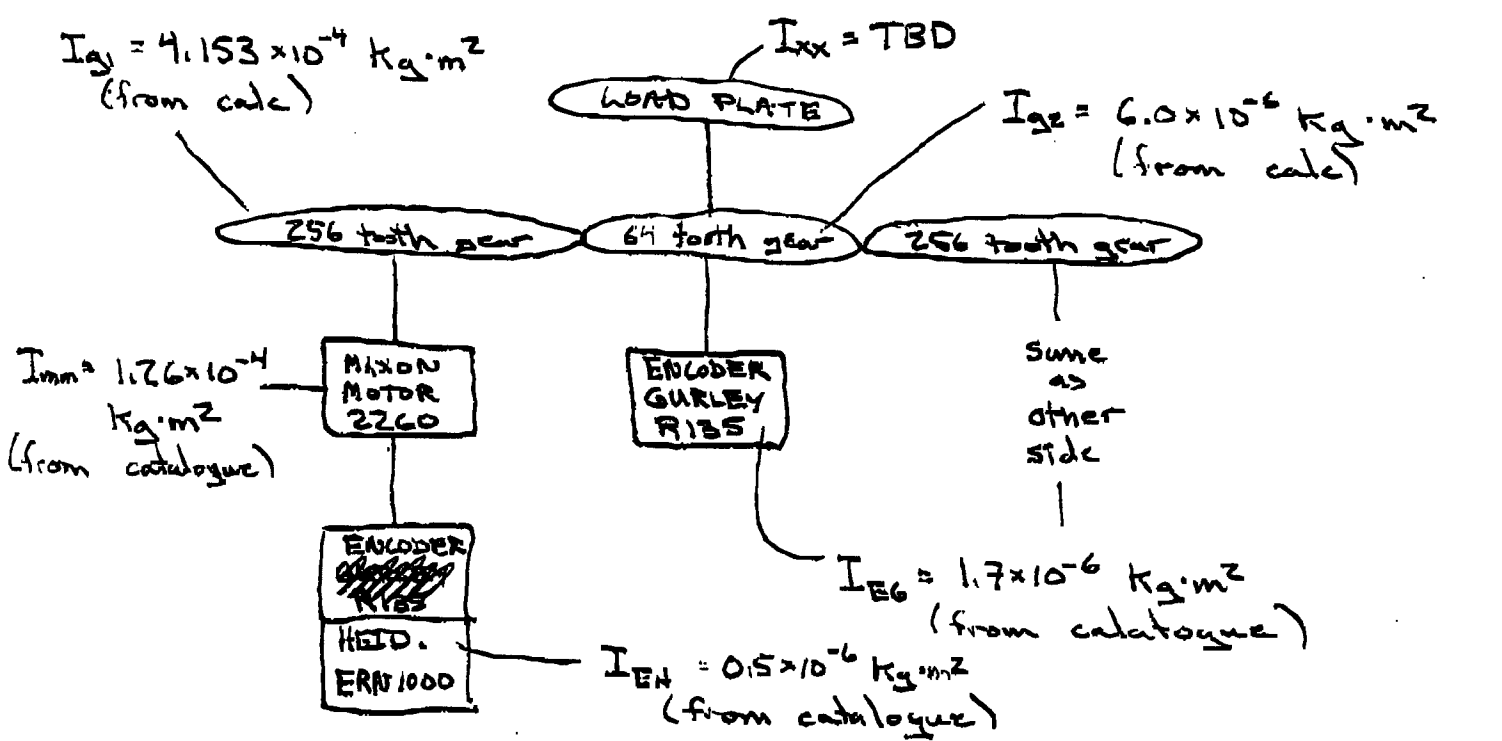
$$\therefore \ddot{\theta}_m = \frac{271}{\{ 1.454 + .250 + 25.690 \}}$$

$$= 9.893 \text{ rad/s} \quad [\text{of motor axis}]$$

REVISED MODEL (Oct 27/03)

- \* now using Gurley RIBS encoders for position
- \* still using Maxon 2260 motors
- \* now using Heidenhain ERN1000 encoders for velocity
- \* still using 256 tooth gear on motor axis
- \* now using 64 tooth gear on load axis

- Gurley RIBS has 230400 counts/rev (e encoder)  
 ∴ has 221600 counts/rev (e motor) ✓



$$\frac{.332}{9.893} = 2 \left[ 1.26 \times 10^{-4} + 0.5 \times 10^{-6} + 4.153 \times 10^{-4} \right] + \left( \frac{256}{64} \right)^2 \left[ 6.0 \times 10^{-6} + 1.7 \times 10^{-6} + I_{xx} \right]$$

$$I_{xx} = 2.035 \times 10^{-3} \text{ kg.m}^2$$

(3)

SOME  $I_{xx}$  Calc for size of tableA disk = Aluminum ( $\rho = 2700 \text{ kg/m}^3$ )

$$\begin{aligned} \text{dia} &= 150 \text{ mm} && (\text{approx } 6") \\ \text{th} &= 6.35 \text{ mm} && (\text{exact } \frac{1}{4} ") \end{aligned}$$

$$\begin{aligned} I_{xx} &= 0.85 \times 10^{-3} \text{ kg}\cdot\text{m}^2 \\ m &= 0.303 \text{ kg} \end{aligned}$$

A disk = Aluminum

$$\begin{aligned} \text{dia} &= 175 \text{ mm} && (\text{approx } 7") \\ \text{th} &= 6.35 \text{ mm} && (\text{exact } \frac{1}{4} ") \end{aligned}$$

$$\begin{aligned} I_{xx} &= 1.58 \times 10^{-3} \text{ kg}\cdot\text{m}^2 \\ m &= 0.412 \text{ kg} \end{aligned}$$

\* I recommend a 7" alum disk,  $\frac{1}{4}$ " thick with a bolt circle pattern @  $\phi 6"$  (maybe 12 holes  $\times \frac{1}{4}$ -20) that you can put SHCSs in to adjust mass.

TACH CALC

Currently : We use T65714 (Inland)

$$12 \text{ Volts / (rad/s)} \Rightarrow .008 \text{ V / (arcsec/sec)} \leftarrow \text{ON SKY}$$

$$\Rightarrow .0000581 \text{ V / (arcsec/sec)} \leftarrow \text{ON MOTOR}$$

But our current noise floor is 1.22 mV

$$\Rightarrow \therefore \text{we currently have } 21 \text{ arcsec/sec} \\ \text{resolution on the motor}$$

$$\Rightarrow \therefore \text{we currently have } .145 \text{ arcsec/sec} \\ \text{resolution on the telescope}$$

$\Rightarrow$  TO GET 20 arcsec/sec resolution on motor

@ 100 Hz readout (.01 s)

$$\begin{aligned} \text{we require } (.01)(20) &= .2 \text{ arcsec resolution on encode} \\ &= 5 \text{ counts / arcsec} \\ &= 6480000 \text{ counts / rev} \end{aligned}$$

$$\begin{array}{l} \text{ERU } 1000 \rightarrow 3600 \text{ lines / rev} \\ \text{IK } 220 \rightarrow 4096 \text{ interp} \end{array} \} \Rightarrow 15782400 \text{ counts / rev}$$

$\Rightarrow$  TRY @ 150 Hz readout ( $5 \times 30 \text{ Hz}$ )  $\Rightarrow \left(\frac{1}{150}\right) \text{ sec / cycle}$

$$15782400 \text{ counts / rev} = 12.178 \text{ counts / arcsec}$$

$$= 0.0821 \text{ arcsec / count}$$

$$\therefore \text{we get } \frac{.0821 \text{ arcsec}}{\left(\frac{1}{150}\right) \text{ sec}} \Rightarrow$$

$$12.31 \text{ arcsec/sec} \\ \text{resolution (on motor)} \\ \text{* better than tach *}$$

## TCS LAB MOTOR - BEARINGS

- \* It will be very important that we remove all axial/radial clearance.
- \* As bearing is mounted on shaft/in housing, an interference fit or transition fit should be used.
- \* Using two "single row angular contact" bearings seated in a back to back arrangement will allow us to remove all clearance as we preload the bearing. SEE pg A-5  
A-20  
A-22
- \* I have selected SINGLE ROW ANGULAR CONTACT
 

Bore	-	10 mm $\phi$	
Housing	-	30 mm $\phi$	COST BETWEEN \$50-200 pr
Width	-	9 mm	
Contact Angle	=	30°	
- \* Bearing tolerance class P4 (ABEC 7) SEE pg A52
- \* Bearing fits to be transition or interference :

∴ on 10 mm shaft we require  $j5 \Rightarrow \begin{matrix} +.003 \\ -.003 \end{matrix}$  mm  
or  $h5 \Rightarrow \begin{matrix} +.000 \\ -.006 \end{matrix}$  mm



I found St. Steel ground shaft 10mm  $\phi$  in the NORDEX catalogue with  $\begin{matrix} +.000 \\ -.005 \end{matrix}$  tolerance and 25 $\mu$ m finish for approx. \$8.00/ft.

LONG LEAD ITEMS

2 x Heidenhain ERN 1000 \$280 ea  
 1 x Heidenhain IR 220 \$1380 ea

(2 x Maxon 2260 motor \$265 ea  
 2 x Maxon Servo Amp \$119 ea

2 x 256 tooth gear \$50 ea  
 1 x Angular contact bearing \$100 ea

Misc hardware (shaft coupling, etc) \$100

(1 x Gurley R135 encoder (220480) \$440  
 2 x Angular Contact bearing \$100  
 1 x 64 tooth gear \$25 ea

Misc hardware (shaft, coupling, etc) \$100

4075

x2 = 8150

Need Computer → OK  
 Need DIA board → \$200<sup>00</sup>

15/10

∴ on 30 mm housing we req. JS6  $\Rightarrow$   $\begin{matrix} +.0065 \\ -.0065 \end{matrix}$

or HG  $\Rightarrow$   $\begin{matrix} +.013 \\ -.000 \end{matrix}$



I would prefer to go with the JS6 tolerance on the hole. i.e. tolerance should read:

30.0  $\begin{matrix} +.0065 \\ -.0065 \end{matrix}$  mm

SEE PG A80-A85

\* TO remove all axial/radial clearance, preload should be applied using a nut, or cap+ bolts capable of adjusting preload in the axial direction. SEE PG A106

